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Conducting nanocomposites based on Polyamide 66 and Carbon Nanofibers prepared by cryogenic grinding

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ABSTRACT

Nanocomposites based on polyamide 6,6 and carbon nanofiber have been obtained following a new procedure. It consists of the physical mixing of the polymer matrix, in the form of powder, and the corresponding amount of additive. Then, samples were prepared by compression moulding and their structural characteristics, as well as their thermal and electrical properties were determined. The materials present good electrical conductivity at lower percolation thresholds than those corresponding to systems prepared by melt mixing. The study was carried out with two different grain sizes, and the findings are discussed in terms of the different size ratios of polymer to carbon nanofiber.

Keywords:

A. Polymer-matrix composites

A. Nano composites

A. Carbon fibers

B. Electrical properties

E. Powder processing

1. Introduction

Conductive composites based on the addition of carbon nanofibers (CNF) to polymeric matrices offer many functional applications in the manufacture of sensors, electromagnetic shielding materials, electrostatically paintable materials, parts for automotive engineering, etc¹. Depending on the additive concentration, the electrical conductivity of a composite material varies from that of the polymer matrix to that one of the carbon additive, due to the formation of a percolative network of the conducting additive at a critical concentration². Percolation at low critical concentration is highly

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desirable in order to remain as close as possible to the mechanical properties of the polymer matrix. The type of polymer, additives themselves, as well as the dispersion method affect the properties of composite materials²¹. Effective utilization of CNF in composites with regard to enhancement of electrical conductivity depends primarily on the ability to disperse the nanoadditive homogeneously in the polymer. The first obstacle to be overcome is the destruction of agglomerates due to the intermolecular van der Waals interactions between CNF. Although, as far as industrial applications are concerned the preferred method is melt mixing, it has been reported the breakage of these nanoadditives during processing³. Accordingly, a reduction of the aspect ratio has to be taken into account because if the aspect ratio becomes lower, the formation of a percolated conductive network requires higher nanoadditive content. In addition, melt mixing very often leads to polymer degradation, as is the case of polyamide 6,6 (PA66). This polymer presents serious drawbacks (water absorption, low melt viscosity, high melting point, etc.) upon processing in the molten state.

In this paper, we present a study of nanocomposite materials based on PA66 and CNF prepared by an alternative procedure, aiming to obtain nanocomposites with good electrical properties at low loadings, without damaging their mechanical properties.

2. Experimental

2.1. Preparation of PA66 nanocomposites

Commercial PA66 (DINALON, REPOL, Spain) and commercial grade CNF (GANF, Antolín Ingeniería, Spain) were used as received. The experimental procedure⁴ involves:

1) Obtaining polymer powder by cryogenic milling. Two sieves were used in order to obtain different powder sizes. Particle size distribution was analyzed with a Mastersizer 2000 (Malvern Instruments Ltd).

2) Physical mixture of polymer powder with the desired amount of CNF, by a vortex mixer Reax Top (Heidolph).

Different composites were prepared by melt mixing using a rheometer Haake PolyLab QC. Temperature was set at 270 °C and rotor speed at 60 rpm; 10 min mixing time sufficed to generate a steady-state torque response.

Then, films of about 1 mm thick were obtained by compression moulding at 280 °C, 15 bar pressure, and subsequent cooling down to room temperature.

2.2. Techniques

TEM and SEM studies were carried out using a Jeol JEM 2010 and a Hitachi S-300N, respectively. Wide angle X-ray scattering measurements were performed by means of a Seifert XRD 3000 θ/θ diffractometer using Ni-filtered Cu K α radiation ($\lambda = 0.154$ nm) at a scanning speed of 0.02 °/s. Differential scanning calorimetry study was carried out using a Perkin-Elmer DSC7 system, under nitrogen environment. The temperature was set from 40 to 330 °C, at the heating rate of 20 °C/min. For the dielectric experiments, a sandwich geometry was used. Measurements were performed, at room temperature, over a frequency window of 10^{-2} - 10^7 Hz, using a Novocontrol spectrometer integrating an ALPHA dielectric interface.

3. Results and discussion

Fig.1 shows TEM micrographs corresponding to the CNF. The characteristic morphology of the nanoadditive consists of a high aspect ratio tubular structure^{5,20} made of rolled graphene layers. Fig.2 shows the particle size distribution corresponding to the two polymer powders. The finest powder exhibits a bimodal distribution with a maximum size around 100 μm , while the highest one presents a maximum around 450 μm . Fig.3A and 3B shows SEM micrographs of nanocomposites with 1 wt% of CNF. In both cases, a tendency to cover the polymer particle in a rather homogenous way is observed.

Fig.4A shows WAXS patterns corresponding to neat PA66 and some of the nanocomposites, after compression moulding. The patterns can be deconvoluted into a broad amorphous halo and three sharper peaks originated by the diffracting planes of the crystalline regions. All samples exhibit the two main peaks corresponding to the α crystalline form of PA66⁶ located at 20.3° and 23.6°. Additionally, the diffractograms exhibit a peak at 26.2° corresponding to the reflection from the graphitic layer structure of the CNF. Fig.4B represents the heating thermograms for the same composites. From these results, it follows that the crystallinity of the polymer matrix does not seem to vary significantly by the presence of the nanoadditives, being the difference among all

samples smaller than 0.3 %. Moreover, the degree of crystallinity determined by WAXS and DSC are of the same order and similar for all samples.

The electrical conductivity as a function of frequency is shown in Fig.5. When the nanoadditive content is below ≈ 6 wt% for PA66-100 μm and ≈ 4 wt% for PA66-450 μm , the dependence of the electrical conductivity with frequency exhibits the characteristic behavior of an insulating material. This follows from a linear dependence of $\log [\sigma (F)]$ with the logarithm of the frequency with a slope close to 1. This behavior is similar to that shown by the PA66 matrix. However, for concentrations higher than the above-referred values, $\sigma (F)$ adopts a different behavior that can be formally described by the so-called universal dynamic response⁷ expressed by a law of the type:

$$\sigma (F) = \sigma_{dc} + \sigma_{ac} = \sigma_{dc} + A F^s \quad (1)$$

where σ_{dc} is the frequency independent direct current conductivity and the exponent s fulfills $0 < s < 1$. This law introduces a critical frequency, F_c , above which $\sigma (F) = \sigma_{ac} \propto F^s$. The continuous lines in Fig.5 correspond to fits of eq.1 to experimental data. From these fits, the σ_{dc} values can be extracted. The value of the conductivity at the lowest measured frequency (10^{-2} Hz) has been considered as the σ_{dc} for the insulating samples.

Fig.6 represents σ_{dc} data as a function of CNF concentration for the two system investigated (conductivity data corresponding to composites prepared from the molten state are also included). In both cases, a characteristic percolative behaviour is observed. According to percolation theory, the insulator-conductor transition occurs at the critical concentration at which an infinite cluster of physically connected particles appears. For low concentrations, the conductivity remains at the same level as the insulating matrix. At a certain critical concentration around 6 wt% for PA66-100 μm and 4 wt% PA66-450 μm , the conductivity starts a sudden increase. The dc conductivity above the critical concentration can be analyzed in terms of the percolation theory^{7,8} by means:

$$\sigma_{dc} \propto (\phi - \phi_c)^t \quad (2)$$

where t is a critical exponent. Although the critical concentration, ϕ_c , depends on the lattice in which particles are accommodated, t depends primarily on the dimensionality of the percolating system and not on the details of the geometric structures or the interactions^{7,8}. Theoretical calculations⁹ propose values of t between 1.6 and 2 for three-dimensional systems. The fitting of eq.2 to experimental data of Fig.6 provides t values

of around 2.7 and 2.4 with $\Phi_c \sim 6$ wt% and 4 wt% for composites based on PA66-100 μm and PA66-450 μm , respectively. Although these values are larger than the generally reported ones, they can be considered as acceptable for a percolative model, since composite materials with high values of the critical exponent have been frequently reported in the literature¹⁰, even deduced from numerical simulation methods when an intercluster polarization is assumed¹¹.

Broadband dielectric measurements also provide information about the ac conductivity as described by the frequency dependent part of eq.1. The results of Fig.5 show that the electrical conductivity remains constant until a certain critical frequency is reached. Moreover, the higher the dc conductivity, the higher the critical frequency. This effect, which has been observed for several disordered materials¹², is described by:

$$F_c \propto \sigma_{dc}^b \quad (3)$$

where the exponent b takes values close to 1. Fig.7 shows F_c as a function of σ_{dc} . The F_c data have been calculated as that frequency at which a 5 % increase in conductivity with respect to the corresponding σ_{dc} value is observed. The power law is rather well fulfilled with an exponent $b \approx 0.9$ for both types of composites. At frequencies $F > F_c$, the conductivity exhibits a frequency dependence that can be described as $\sigma_{ac} \propto F^s$. Fig.8 shows the variation of F_c and s , as obtained from the fitting of eq.1, with CNF content. As seen, $\log F_c$ increases linearly with carbon nanoadditive content, whereas s -exponent starts from 1 and then a decrease is observed.

By simulation studies Bergman and Imry¹³ showed that the variation with frequency, in the percolation concentration vicinity, of the ac conductivity and dielectric constant of a heterogeneous mixture might be described by a power law at frequencies $F > F_c$:

$$\sigma_{ac}(F, \Phi_c) \sim F^x \quad (4)$$

$$\epsilon'_{ac}(F, \Phi_c) \sim F^y \quad (5)$$

these critical exponents, x and y , are supposed to satisfy:

$$x + y = 1 \quad (6)$$

It is to be noted that the exponent x is equal to s in the Jonscher equation (see eq.1). Fig.9 shows data of ac conductivity and dielectric constant, versus frequency, near the percolation threshold. The results are in good agreement with the above general scaling relation (eq.6). For three-dimensional materials, it has been proposed x values

ranging from ≈ 0.72 , when the frequency dependence of these functions has been attributed to the polarization effects between clusters in the matrix¹⁴, to ≈ 0.58 when anomalous diffusion within each percolating cluster is proposed¹⁵. From our results, we conclude that the values found for both systems are closer to the predictions of the intercluster polarization model.

Regarding these results, one aspect to be emphasized is the low percolation thresholds if compared with those reported for similar systems, but prepared by melt mixing^{16,17} (see also Fig.6). Assuming that by this procedure the carbon nanofiber breakage does not take place, or at least it would be not so severe as in the case of melt mixing, a plausible explanation to that fact could be that the PA66 solid particles create volume excluded, reducing the space available to form conductive paths, and pushing CNF into the interstitial spaces. Under this circumstance, composites present a segregated structure of CNF, which are located on the surface of the polymer, coating the particles, instead of being randomly distributed in the whole system. Although for very different systems, a quite similar behavior has been reported^{18,19}. This arrangement is supposed to act as a footprint during the compression molding as it is shown schematically in Fig.10. Another important aspect worthy to be mentioned is the fact that when the grain size is larger, the percolation threshold is significantly lower. This behavior, which has already been described for other type of systems¹⁸, can be attributed to the fact that when the ratio of the particle size of polymer to nanoadditive is high enough, the coating process is more effective and the arrangements of CNF in the segregated phase are more appropriate to form the network of connected particles.

4. Conclusions

In this work, we carry out the structural characterization as well as the study of electrical properties of systems based on PA66 and CNF and prepared by an alternative procedure to melt processing. The method consists of the physical mixture of the polymer matrix, in the powder form, and the nanoadditive, by a vortex mixer. The study was performed using two polymer particle sizes. From the results, it can be inferred that this method yields materials without significant variation in their structural characteristics, being all composites similar to neat PA66. Regarding electrical conductivity, the materials based on both particle sizes have good electrical conductivity

and show lower percolation thresholds than those composites processed from the molten state. One explanation for that fact could be that PA66 solid particles create excluded volume and push CNF into the interstitial space. Under this circumstance, CNF form a segregated distribution of the nanoadditive, which ultimately act as a precursor for the formation of the physical network between particles. However, there are differences between both particle sizes. In spite of the final conductivity value reached by both systems is of the same order, the percolation threshold is lower in the case of the highest polymer particle size. The reason could be that in the case of the highest particle size, the coating process of polymer particles by carbon nanofibers is more effective and the arrangements of CNF in the segregated phase are more appropriate to form the network of connected particles, which is characteristic of percolative behavior.

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Legends to the figures

Fig.1.- TEM images of CNF. The background honeycomb-like structure is due to the TEM grid.

Fig.2.- Particle size distribution of both PA66 powders used in this study.

Fig.3.- SEM images of A: PA66-100 μm and B: PA66-450 μm with 1 wt% of CNF.

Fig.4.- WAXS patterns (A) and DSC-curves (B) corresponding to: a: PA66-100 μm +3.5% CNF; b: PA66-100 μm +8% CNF; c: PA66-450 μm +5% CNF and d: PA66-450 μm +11% CNF. The different contributions in which WAXS patterns can be decomposed are shown in the figure.

Fig.5.- Broadband electrical conductivity as a function of frequency. The continuous lines represent fits according to eq.1.

Fig.6.- Electrical conductivity versus nanoadditive concentration. Continuous lines are the fitting of eq. 2. Data corresponding to composites obtained by melt mixing are also included (\blacktriangle).

Fig.7.- Logarithm of the critical frequency versus the logarithm of σ_{dc} .

Fig.8.- Logarithm of the critical frequency and exponent s according to eq.1 as a function of CNF content.

Fig.9.- Dependence of ac conductivity and dielectric constant with frequency near percolation threshold. Open symbols correspond to PA66-100 μm and solid symbols to PA66-450 μm nanocomposites.

Fig.10.- Scheme of compaction of PA66 particles with CNF at different polymer grain size. A: 450 μm and B: 100 μm .



















